## Numerical study of H<sub>2</sub>S-H<sub>2</sub>O-air mixture conversion to hydrogen via activation of air by an electric discharge

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Hydrogen sulfide, which is a part of associated petroleum and so-called acid natural gases and which forms from the sulfur-containing fuels in petroleum refining industries, can serve as a source of hydrogen that is considered lately as an energy efficient and environmentally safe fuel. The direct conversion of  $H_2S$  to  $H_2$  occurs only at rather high temperature, and such a process requires a fairly large amount of heat to be supplied to the system. For the implementation of low-temperature conversion of  $H_2S$ , an approach based on the partial oxidation of  $H_2S$  upon activation of the oxidizer (air) by an electric discharge is considered in this work.

Numerical study is carried out in an adiabatic flow reactor with the length of L=1 m at pressure P=1 atm and inlet gas velocity  $U_0=1$  m/s, which corresponds to the gas residence time in the reactor of  $\tau_r \sim 1$  s. Air, activated in an electrical discharge, and H<sub>2</sub>S-H<sub>2</sub>O mixture are supplied to the flow reactor inlet separately, where they mix and the homogeneous mixture moves in the reactor. Both flows are preliminarily heated up to the temperature  $T_0=500$  K, the reduced electric field E/N in the discharge varies in the range of 1-150 Td (1 Td= $10^{-17}$  V·cm<sup>2</sup>), the specific energy put into the discharge is  $E_s=0.3-0.5$  J/ncm<sup>3</sup>, fuel-to-oxidizer equivalence ration was chosen to be  $\phi=2$ , basing on the preliminary thermodynamic analysis, according to which, for such  $\phi$  value, a maximum or close to the maximum yield of H<sub>2</sub> in H<sub>2</sub>S-air mixture is realized.

Calculations have shown that a significant amount of H<sub>2</sub> is formed only after the H<sub>2</sub>S-H<sub>2</sub>O-air mixture ignites. At  $E_s=0.5$  J/ncm<sup>3</sup>, the mixture with a fraction of water vapor  $\varepsilon = n_{H_2O}^0 / n_{H_2S}^0 = 0-1$  ( $n_{H_2O}^0$  and  $n_{H_2S}^0$  are the molar flow rates of H<sub>2</sub>O and H<sub>2</sub>S at the reactor inlet) ignites inside the reactor for any *E/N* value. But the shortest ignition length is realized for the discharge, producing maximum amount of O<sub>2</sub>( $a^1\Delta_g$ ) molecules. The values *E/N*~4–10 and 120–150 Td are most favorable. At  $E_s=0.3$  J/ncm<sup>3</sup>, the mixture ignites only at  $\varepsilon=0-0.2$  and only at the *E/N* values, when the molar fraction of O<sub>2</sub>( $a^1\Delta_g$ ) molecules is maximal. If the mixture ignites inside the reactor, H<sub>2</sub> yield does not depend on *E/N*. With an increase of the amount of H<sub>2</sub>O in the mixture and a reduction of the energy  $E_s$ , supplied into the discharge, the range of *E/N* values, at which H<sub>2</sub>S conversion occurs, narrows. On the other hand, the addition of water vapor leads to an increase of the relative yield of hydrogen  $\delta = n_{H_2} / n_{H_2S}^0$  ( $n_{H_2}$  is the molar flow rate of H<sub>2</sub> at reactor exit) from 0.25 to 0.3 when  $\varepsilon$  varies from 0 to 1.

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